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102 27 012.0 18. Juni 2002 (18.06.2002) DE(71) Anmelder (für alle Bestimmungsstaaten mit Ausnahme von  
US): ROBERT BOSCH GMBH [DE/DE]; Postfach 30 02  
20, 70442 Stuttgart (DE).

(72) Erfinder; und

(75) Erfinder/Anmelder (nur für US): SCHUMANN, Bernd  
[DE/DE]; Hegelstr. 34, 71277 Rutesheim (DE).(74) Gemeinsamer Vertreter: ROBERT BOSCH GMBH;  
Postfach 30 02 20, 70442 Stuttgart (DE).

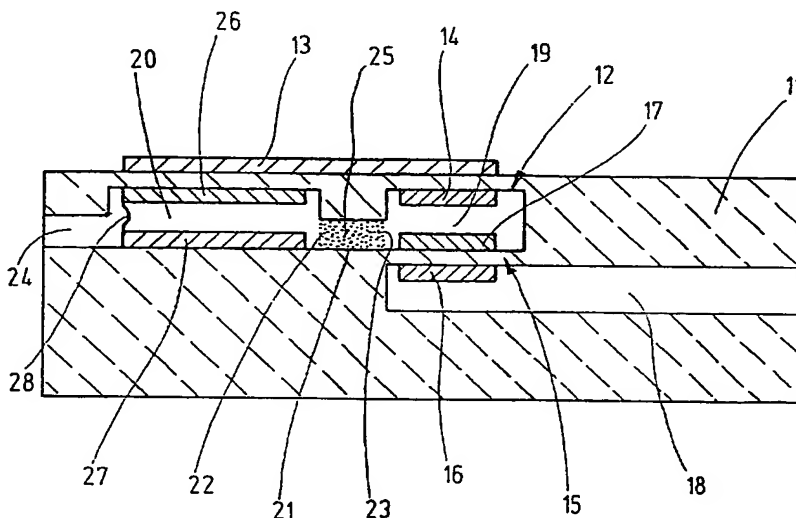
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HAUST GAS OF INTERNAL COMBUSTION ENGINES(54) Bezeichnung: SENSORELEMENT FÜR EINEN MESSFÜHLER ZUR BESTIMMUNG DER SAUERSTOFFKONZENT-  
RATION IM ABGAS VON BRENNKRAFTMASCHINEN

(57) **Abstract:** The invention relates to a sensor element for a sensor for determining the oxygen concentration in the exhaust gas of internal combustion engines, in particular for a broadband lambda probe. Said element comprises: a solid electrolyte (11), which forms a pump cell (12) with an internal electrode (14) located in a hollow chamber and an external electrode (13) that is exposed to the exhaust gas; an antechamber (20) that is configured in the solid electrolyte (11); and a diffusion channel (21) that is configured in the solid electrolyte (11), interconnects the antechamber (20) and hollow chamber (19) and is filled with a diffusion barrier (25). In order to prevent measuring inaccuracies of the sensor in the presence of extremely high quantities of hydrocarbons in the exhaust gas, a catalyst for oxidising hydrocarbons is located in the antechamber (20), said catalyst being configured in a preferred embodiment as an electrochemical catalyst comprising two electrically connected electrodes (26, 27).

[Fortsetzung auf der nächsten Seite]

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SENSOR ELEMENT FOR A SENSOR FOR DETERMINING THE OXYGEN  
CONCENTRATION IN THE EXHAUST GAS OF INTERNAL COMBUSTION  
ENGINES

Background Information

The present invention is directed to a sensor element for a  
sensor for determining the oxygen concentration in the  
5 exhaust gas of internal combustion engines, in particular  
for a broadband lambda sensor, according to the  
characterizing portion of Claim 1.

In a known sensor element for a lambda sensor for  
10 determining the lambda-value as a measure of the oxygen  
concentration in the exhaust gas of the internal combustion  
engine (DE 198 57 471 A1), the cavity accommodating the  
inner electrode of the pump cell, the diffusion chamber  
along with the diffusion barrier, and the prechamber are  
15 configured in a circle around a hole drilled into the ion-  
conducting solid electrolyte, preferably made of zirconium  
oxide ( $ZrO_2$ ), so that the prechamber has a cylindrical  
access opening for the exhaust gas, and the diffusion  
channel has a cylindrical intake opening from the direction  
20 of the prechamber and a cylindrical exit opening toward the  
cavity. The prechamber, here, has only a small radial depth,  
at least big enough so that the drill making the hole in the  
solid electrolyte does not touch the inner cylinder wall of  
the diffusion barrier during the drilling process clogging  
25 the pores of the diffusion barrier, which could result in a  
change in the diffusion resistance of the diffusion barrier.

In the case of large proportions of unburned or partially

burned hydrocarbons in the exhaust gas such as develop during fuel post-injection for soot filter regeneration in diesel engines, the measuring accuracy of the sensor is negatively affected by the different diffusion coefficients of hydrocarbons and oxygen as they pass through the diffusion barrier. Depending on the type of hydrocarbons, they have molecules of varying sizes and therefore diffusion coefficients which are larger or smaller than or equal to that of oxygen. High molecular weight hydrocarbons such as decane permeate the diffusion barrier at a much lower rate than oxygen, so that - per time unit - significantly less hydrocarbon passes through the diffusion barrier and enters the cavity. In the cavity of the pump cell, less oxygen is consumed after the reaction of the hydrocarbons with oxygen than would be expected stoichiometrically given the concentration of the gas fractions in the exhaust gas. The sensor, in other words, measures too high of an oxygen concentration. Conversely, low molecular weight hydrocarbons such as methane permeate the diffusion barrier at a higher rate than oxygen. More hydrocarbons therefore enter the cavity and react with more oxygen than would be expected given their concentration in the exhaust gas. The sensor therefore measures too low of an oxygen concentration.

## Advantages of the Invention

The sensor element according to the present invention, having the characteristics of Claim 1, has the advantage that the catalytic converter upstream of the diffusion barrier causes the hydrocarbons to oxidize more efficiently. The exhaust gas volume entering the cavity through the diffusion barrier thus does not contain any unburned hydrocarbons having diffusion coefficients deviating from the diffusion coefficient of the oxygen, so that the stoichiometric ratio of the oxygen is set upstream from the

diffusion barrier and is not changed again in the exhaust gas volume present in the cavity; in other words, the sensor delivers correct lambda values.

5     Advantageous refinements of and improvements on the sensor element cited in Claim 1 are possible via the measures listed in the dependent Claims.

10     According to a preferred embodiment of the present invention, the catalytic converter is operated as an electrochemical catalytic converter in the prechamber, for which purpose spatially distanced and electrically connected electrodes made of an electrically conductive material essentially containing a precious metal such a platinum,  
15     rhodium, palladium and/or an alloy thereof, are placed on two opposing chamber walls, and where the electrode material may have an oxidation-promoting oxide such as aluminum oxide or cerium oxide added to it.

20     According to alternative embodiments of the present invention, the electrochemical catalytic converter may be connected - either permanently or for a limited time such as only during fuel post-injection - to a DC voltage, or the electrical conductivity of the prechamber electrodes may be  
25     used simply for the purpose of having the electrodes function as a catalytic converter. In the former case, the prechamber electrodes are operated such that oxygen is electrochemically pumped into the prechamber, where the oxygen efficiently oxidizes the hydrocarbons. For this  
30     purpose, an anodic current is applied to the prechamber electrodes, for which purpose the prechamber electrodes are connected to a DC voltage having a higher potential than that of the outer electrodes of the pump cell. In the latter case of forming, a cathodic current is applied to the  
35     prechamber electrodes, with the prechamber electrodes being

subjected to a lower potential than that of the outer electrodes of the pump cell. This cathodic current flows for a few minutes at a voltage higher than the decomposition voltage of the solid electrolyte material, resulting in the electrochemical formation - on the surface of the prechamber electrodes - of a cermet from the electrode metal and the zirconium oxide of the solid electrolyte, imparting to the prechamber electrodes a very good catalytic activity. Here, the sensor element is preferably subjected to a temperature between 800°C and 1200°C.

Forming of the catalytic converter takes place according to the sintering process of the sensor element and may remain restricted to a one-time forming. In this case, it is not necessary to run a connecting cable from the sensor element to the prechamber electrodes, since these prechamber electrodes may be contacted through the access opening in the prechamber in the case of a one-time forming. It is also possible, however, to carry out the forming of the catalytic converter in the prechamber repeatedly from time to time, even while the sensor is being used. In this case, a connecting cable leading to the prechamber electrodes must be provided and connected to the control unit of the sensor.

## Drawing

The present invention is described in greater detail with reference to an exemplary embodiment. The drawing is a schematic representation of a cross section of a sensor element for a sensor configured as a broadband lambda sensor.

## Description of the Exemplary Embodiment

The sensor element for a sensor configured as a broadband

lambda sensor for determining the oxygen concentration in the exhaust gas, schematically sketched in the drawing, has solid electrolyte 11 forming the sensor body, where solid electrolyte 11 is made of yttrium-stabilized zirconium oxide, for instance, and is usually composed of several ceramic layers joined by a sintering process. The individual ceramic layers are not shown here.

Solid electrolyte 11 contains a pump cell 12 which operates on the limit current principle, and has outer electrode 13 and inner electrode 14, as well as a measuring cell or Nernst cell 15 having a reference electrode 16 and a Nernst electrode or measuring electrode 17. Reference electrode 16 is located in a reference channel 18 formed in solid electrolyte 11, with a reference gas, preferably air, admitted to reference channel 18. Alternatively, it is also possible to generate the reference gas atmosphere electrochemically, in which case reference channel 18 is replaced by a barely gas-permeable layer. Solid electrolyte 11, furthermore, contains cavity 19, prechamber 20 upstream from cavity 19, and diffusion channel 21 connecting prechamber 20 with cavity 19, diffusion channel 21 having an intake opening 22 toward prechamber 20, and an exit opening 23 toward cavity 19. Prechamber 20 has an access opening 24, through which exhaust gas may enter prechamber 20. Diffusion channel 21 is filled with diffusion barrier 25, made of aluminum oxide ( $\text{Al}_2\text{O}_3$ ) or zirconium oxide ( $\text{ZrO}_2$ ), for instance, and has a given diffusion resistance. The barrier material may also have catalytically active material added to it. Measuring electrode 17 of Nernst cell 15, and inner electrode 14 of pump cell 12 are installed spatially-distanced in cavity 19. Measuring electrode 17 and inner electrode 14 may be connected electrically and mechanically. The geometric layout of cavity 19 and reference channel 18 is designed such that reference electrode 16 and measuring

electrode 17 of Nernst cell 15, and inner electrode 14 and outer electrode 13 of pump cell 12 are separated from each other by solid electrolyte 11. Outer electrode 13 is situated on the surface of solid electrolyte 11 and is exposed to the exhaust gas when the sensor is in use. Access opening 24 of prechamber 20 is configured such that the access cross section of prechamber 20 for the exhaust gas is much larger than the access cross section of diffusion barrier 25, and at least large enough so that the access cross section of prechamber 20 only slightly increases the diffusion resistance of diffusion barrier 25 for the exhaust gas. Normally, a resistance heater, mounted on a support, is additionally connected to solid electrolyte 11 to heat the sensor element to the required operating voltage. This resistance heater is not shown here.

As discussed previously, a high fraction of unburned or partially-burned hydrocarbons in the exhaust gas impairs the measuring accuracy of the sensor element, resulting in measuring errors in the lambda value. To prevent this measuring error, a catalytic converter for the oxidation of hydrocarbons is located in prechamber 20. This catalytic converter may be a purely chemical catalytic converter, with prechamber 20 filled with a packing of an oxidation-promoting catalyst material. Zirconium oxide ( $\text{ZrO}_2$ ), platinum (Pt), rhodium (Rh) and palladium (Pd) are suitable catalyst materials.

In the above-presented embodiment of the sensor element, the catalytic converter is operated as an electrochemical catalytic converter, with two electrodes 26 and 27 made of an electrically conducting material, installed on two opposing walls of prechamber 20. The chamber walls supporting electrodes 26, 27 are aligned parallel to each other and extend parallel to the center axes of access

opening 24 and intake opening 22 which, in turn, are aligned with each other. The electrode material is essentially precious metal such as platinum, rhodium, palladium and/or an alloy thereof, and where an oxidation-promoting oxide such as zirconium oxide ( $\text{ZrO}_2$ ), zeolite, aluminum oxide ( $\text{Al}_2\text{O}_3$ ) or cerium oxide ( $\text{Ce}_2\text{O}_3$ ) may be added to improve the catalytic effect. The two electrodes 26, 27 are connected with one another in an electrically conductive manner, symbolized in the drawing by connecting wire 28. During operation of the sensor, electrodes 26, 27 are connected to a DC potential which is higher than that of outer electrode 13 of pump cell 12. This causes oxygen ions to be electrochemically pumped from solid electrolyte 11 into prechamber 20, efficiently oxidizing the hydrocarbons contained in the exhaust gas volume entering prechamber 20. No unburned hydrocarbons penetrate diffusion barrier 25, and the stoichiometric ratio of the oxygen concentration in cavity 19 is not distorted. Application of DC voltage may be permanent or occur only during those operational phases of the internal combustion engine, where a particularly high proportion of unburned or partially burned hydrocarbons is generated such as during fuel post-injection for soot filter regeneration or for heating the exhaust gas catalytic converter.

During electrical operation of the electrochemical catalytic converter, part of the oxygen electrically generated in prechamber 20 exits back into the exhaust gas via access opening 24. This fraction, however, is numerically determinable through measurements in gas test benches, and is taken into consideration when calculating the actual oxygen content in the exhaust gas from the current signal of pump cell 12.



In an alternative embodiment of the sensor element, the electrochemical catalytic converter in prechamber 19 is not operated electrically; instead, the electrical conductivity of electrodes 26, 27 is used to form electrodes 26, 27 as catalytic converters, since electrodes 26, 27 are generally produced by cofiring and have poor catalytic activity because of the high sintering temperatures to which the sensor element is exposed during manufacture. For the purpose of forming the catalytic converter, electrodes 26, 27 are connected for several minutes to a voltage above that of the decomposition voltage of the zirconium oxide of solid electrolyte 11 such as 1.3 V - 2 V relative to reference air, so that a cathodic current flows through electrodes 26, 27 and the sensor element is exposed to a temperature between 800°C and 1200°C. During this process, a cermet forms electrochemically on the surface of electrodes 26, 27 from the electrode material and the zirconium oxide, which exhibits high catalytic activity. This forming process may be carried out one single time after sintering of the sensor element, but may also be performed repeatedly when the sensor is in use. In the latter case, a connecting wire leading to electrodes 26, 27 must be run out of the sensor element.

The present invention is not limited to the above-described sensor element for a broadband lambda sensor having pump cell 12 and Nernst cell 15. The sensor element may also be used as a sensor configured as a linear air/fuel sensor, in which case Nernst cell 15 along with its reference electrode 16 and measuring electrode 17, as well as reference channel 18 are not needed. This sensor element, only containing pump cell 12, also operates on the limit current principle.

Furthermore, it is possible to additionally fill the space between electrodes 26, 27 in prechamber 20 with a

catalytically active material. The material used for this purpose may again be  $\text{ZrO}_2$ , Pt, Rh, Pd - as in the case of the chemical catalytic converter in prechamber 20 described above.